

Optimal synthesis of membrane filtration systems

Rémy Dutto ^{1,2} Jérôme Harmand ¹ Alain Rapaport ²

¹LBE INRAE, Narbonne

²MISTEA INRAE, Montpellier

Journées SMAI-MODE 2026, Nice



Introduction

We are interested in :

- membrane filtration systems
- optimal feedback synthesis
- automatic generation

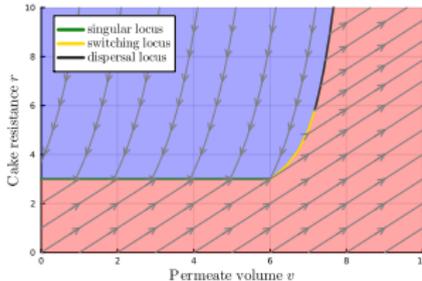


Table of Contents

- 1 Application
- 2 Objectives
- 3 Indirect method
- 4 Optimal synthesis
- 5 Conclusion

Membrane filtration systems

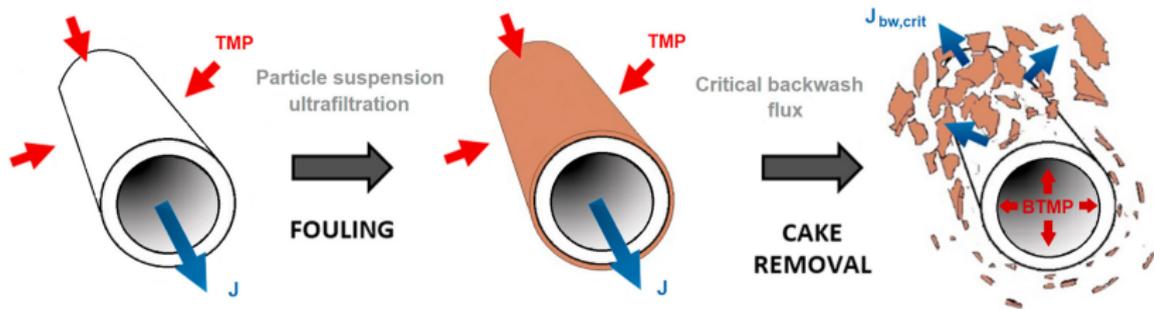


Figure: Extracted from [Vroman et al., 2021]

State/cost :

- r : resistance of cake layer
- v : permeate volume
- e : energy spend

Control :

- $u = +1$: filtration
- $u = -1$: backwash

Dynamics modeling

The dynamics for filtration and backwash modes are assumed to be given respectively by

- $r_+(r)$ and $r_-(r)$ for \dot{r} (speed of variation of r),
- $v_+(r)$ and $v_-(r)$ for \dot{v} (effective flow rate),
- $e_+(r)$ and $e_-(r)$ for \dot{e} (instantaneous energy consumption).

Considering $u \in [-1, 1]$, the dynamics are modeled by

$$\begin{cases} \dot{r} = \frac{1+u}{2}r_+(r) + \frac{1-u}{2}r_-(r), \\ \dot{v} = \frac{1+u}{2}v_+(r) + \frac{1-u}{2}v_-(r), \\ \dot{e} = \frac{1+u}{2}e_+(r) + \frac{1-u}{2}e_-(r). \end{cases}$$

Dynamics modeling

Denoting

$$\begin{aligned}r_0(r) &= \frac{1}{2}(r_+(r) + r_-(r)), & r_1(r) &= \frac{1}{2}(r_+(r) - r_-(r)), \\v_0(r) &= \frac{1}{2}(v_+(r) + v_-(r)), & v_1(r) &= \frac{1}{2}(v_+(r) - v_-(r)), \\e_0(r) &= \frac{1}{2}(e_+(r) + e_-(r)), & e_1(r) &= \frac{1}{2}(e_+(r) - e_-(r)),\end{aligned}$$

the dynamic of the system is

$$\begin{cases} \dot{r} = r_0(r) + u r_1(r) \\ \dot{v} = v_0(r) + u v_1(r) \\ \dot{e} = e_0(r) + u e_1(r) \end{cases}$$

Case #1 : Minimum energy

The goal is to minimise the energy to provide a desired volume of filtered water v_f :

$$(\#1) \quad \left\{ \begin{array}{l} \min_{r, v, u, t_f} \int_{t_0}^{t_f} e_0(r(t)) + u(t) e_1(r(t)) dt, \\ \text{s.c. } \dot{r}(t) = r_0(r(t)) + u(t) r_1(r(t)), \\ \dot{v}(t) = v_0(r(t)) + u(t) v_1(r(t)), \\ u(t) \in [-1, 1], \quad t \in [t_0, t_f], \\ r(t_0) = R_0, \quad v(t_0) = 0, \quad v(t_f) = v_f. \end{array} \right.$$

Case #2 : Maximum volume

The goal is to maximise the filtered volume on a fixed time interval $[t_0, T]$:

$$(\#2) \quad \left\{ \begin{array}{l} \max_{r,u} \int_{t_0}^T v_0(r(t)) + u(t) v_1(r(t)) dt, \\ \text{s.c. } \dot{r}(t) = r_0(r(t)) + u(t) r_1(r(t)), \\ u(t) \in [-1, 1], \quad t \in [t_0, T], \\ r(t_0) = R_0 \geq 0. \end{array} \right.$$

Equivalent formulation

Let us consider the following general formulation

$$(OCP) \quad \left\{ \begin{array}{l} \min_{x,y,u,t_f} \int_{t_0}^{t_f} f_0(x(t)) + u(t) g_0(x(t)) dt, \\ \text{s.c. } \dot{x}(t) = f_1(x(t)) + u(t) g_1(x(t)), \\ \quad \dot{y}(t) = f_2(x(t)) + u(t) g_2(x(t)), \\ \quad u(t) \in [-1, 1], \quad t \in [t_0, t_f], \\ \quad x(t_0) = x_0, \quad y(t_0) = y_0, \quad y(t_f) = y_f, \end{array} \right.$$

and we denote $f = (f_0, f_1, f_2)$ and $g = (g_0, g_1, g_2)$. This problem corresponds to a class of production-regeneration systems where:

- x corresponds to the internal resistance,
- y model a target to reach or a budget constraint.

Equivalent formulation

Case (#1) can be written as (OCP) :

$$(OCP) \quad \left\{ \begin{array}{l} \min_{x,y,u,t_f} \int_{t_0}^{t_f} e_0(x(t)) + u(t) e_1(x(t)) dt, \\ \text{s.c. } \dot{x}(t) = r_0(x(t)) + u(t) r_1(x(t)), \\ \quad \dot{y}(t) = v_0(x(t)) + u(t) v_1(x(t)), \\ \quad u(t) \in [-1, 1], \quad t \in [t_0, t_f], \\ \quad x(t_0) = R_0, \quad y(t_0) = 0, \quad y(t_f) = v_f, \end{array} \right.$$

with $f = (e_0, r_0, v_0)$ and $g = (e_1, r_1, v_1)$. In this case :

- x corresponds to the resistance of the cake layer,
- y corresponds to the produced volume.

Equivalent formulation

Case (#2) can be written as (OCP) :

$$(OCP) \quad \left\{ \begin{array}{l} \min_{x,y,u,t_f} \int_{t_0}^{t_f} -v_0(x(t)) - u(t) v_1(x(t)) dt, \\ \text{s.c. } \dot{x}(t) = r_0(x(t)) + u(t) r_1(x(t)), \\ \dot{y}(t) = 1, \\ u(t) \in [-1, 1], \quad t \in [t_0, t_f], \\ x(t_0) = R_0, \quad y(t_0) = t_0, \quad y(t_f) = T, \end{array} \right.$$

with $f = (-v_0, r_0, 1)$ and $g = (-v_1, r_1, 0)$. In this case :

- x corresponds to the resistance of the cake layer,
- y corresponds to the time.

Objectives

Provide optimal synthesis of (OCP) “whatever” inputs functions and initial/final conditions are.

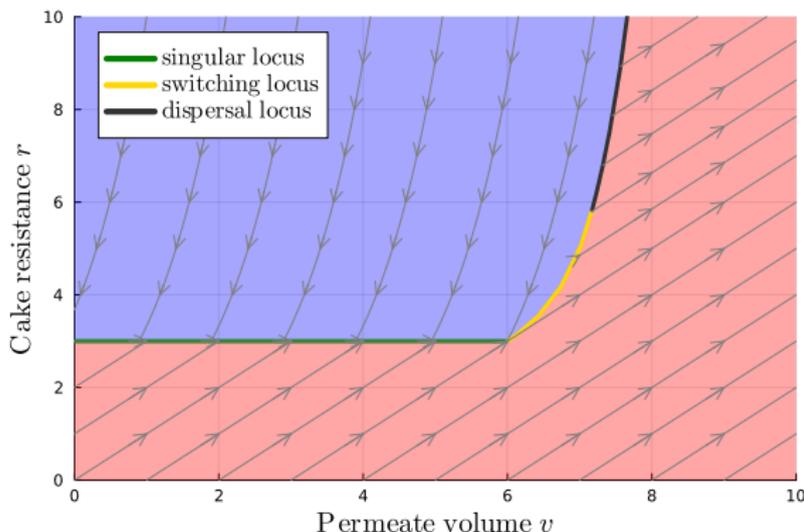


Figure: Example of optimal synthesis with trajectories for Case (#1).

Pontryagin maximum principle

If (x, y, u, t_f) is a solution of (OCP), there exists a costate $p = (-1, p_x, p_y)$ such that $p_x(t_f) = 0$, the *costate dynamic* is satisfied for almost every $t \in [t_0, t_f]$

$$\dot{p}_x(t) = -\frac{\partial H}{\partial x}(x(t), p(t), u(t)), \quad \dot{p}_y(t) = 0,$$

as well as the *maximisation condition* for almost every $t \in [t_0, t_f]$

$$\max_{w \in [-1, 1]} H(x(t), p(t), w) = H(x(t), p(t), u(t)) = 0$$

where H is the *hamiltonian* given by

$$H(x, p, u) = H_0(x, p) + u H_1(x, p),$$

$$H_0(x, p) = \langle p \mid f(x) \rangle \quad \text{and} \quad H_1(x, p) = \langle p \mid g(x) \rangle$$

Optimal control

Using the maximisation condition and the definition of H , for almost all $t \in [t_0, t_f]$, one has

$$u(t) \begin{cases} = -1 & \text{if } H_1(x(t), p(t)) < 0 \\ \in [-1, 1] & \text{if } H_1(x(t), p(t)) = 0 \\ = 1 & \text{if } H_1(x(t), p(t)) > 0 \end{cases}$$

Lemma 1

There exists $\bar{t} \in [t_0, t_f[$ such that $u(t) = 1$ for almost every $t \in [\bar{t}, t_f]$.

Singular state and singular control

Let us suppose that there exists $I \subset [t_0, t_f]$ of non-zero measure such that $H_1(x(t), p(t)) = 0$ for all $t \in I$. One has

$$H_0(x(t), p(t)) = H_1(x(t), p(t)) = 0, \quad (1)$$

$$\frac{d}{dt} H_1(x(t), p(t)) = [H_0, H_1](x(t), p(t)) = 0, \quad (2)$$

where $[\cdot, \cdot]$ corresponds to the Poisson bracket. From (1), one has $p_x(t) = \alpha(x(t))$ and $p_y(t) = \beta(x(t))$ for all $t \in I$ where

$$\Delta(x) \alpha(x) = f_0(x)g_2(x) - f_2(x)g_0(x),$$

$$\Delta(x) \beta(x) = f_1(x)g_0(x) - f_0(x)g_1(x),$$

$$\Delta(x) = f_1(x)g_2(x) - f_2(x)g_1(x).$$

Singular state and control

By using (2) and expression of p_x and p_y , the singular state x_s is constant and must be a zero of

$$\psi(x) = -\beta'(x)\Delta(x). \quad (3)$$

Since the singular state is constant, the singular control cancels \dot{x} and is thus given by

$$u_s = -\frac{f_1(x)}{g_1(x)}.$$

Main theorem

Theorem 2

Under some hypothesis, and denoting

- σ_- an arc associated to $u = -1$,
- σ_+ an arc associated to $u = +1$,
- σ_s an arc associated to $u = u_s$,

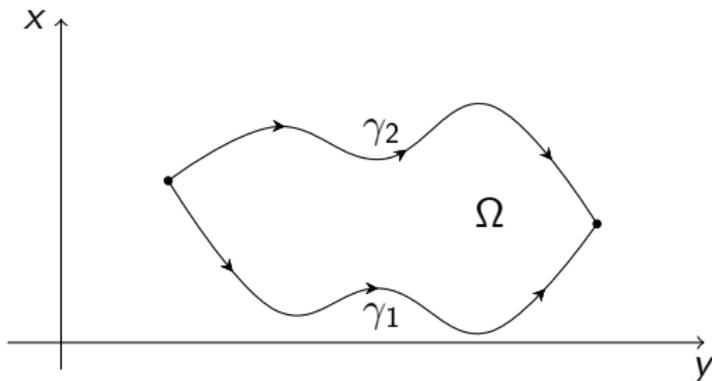
the structure of an optimal solution can only be one of

$$\sigma_+, \sigma_- \sigma_+, \sigma_s \sigma_+, \sigma_- \sigma_s \sigma_+ \text{ or } \sigma_+ \sigma_s \sigma_+.$$

Use of the Green's theorem

By using the state dynamics, one can construct the 1-form

$$(f_0(x) + u(t)g_0(x)) dt = \alpha(x) dx + \beta(x) dy$$



By using the Green's theorem [Miele, 1962], one has

$$J(\gamma_1) - J(\gamma_2) = \oint_{\gamma_1 \cup \gamma_2^{-1}} \alpha(x) dx + \beta(x) dy = \iint_{\Omega} -\beta'(x) dy dx.$$

Optimal synthesis

By finding zero of ψ , one can compute the singular curve

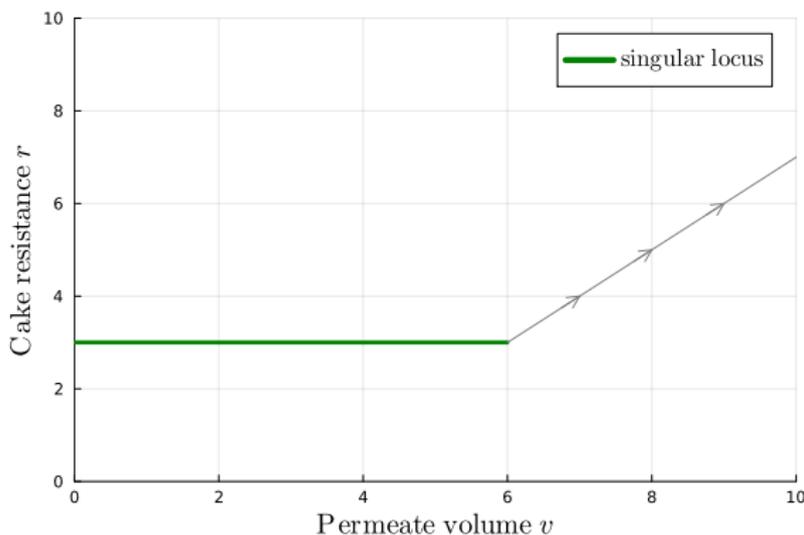


Figure: Optimal synthesis construction

Optimal synthesis

We have to compute the switching curve \mathcal{S}

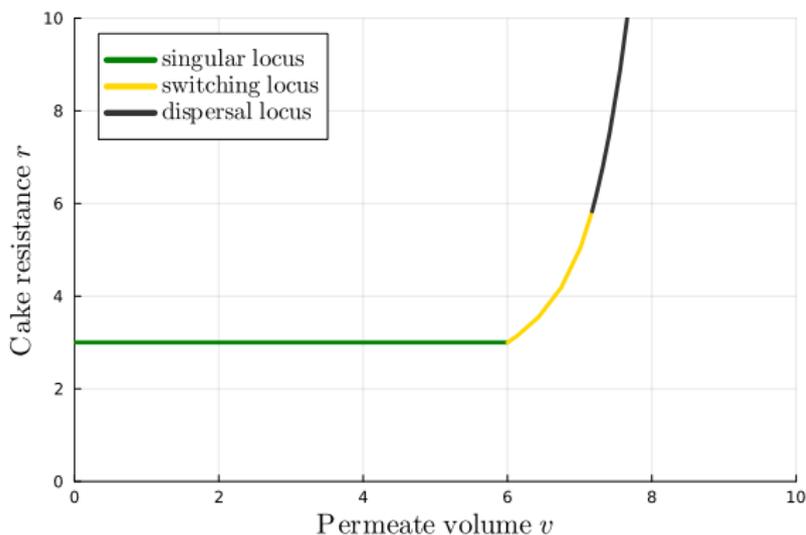


Figure: Optimal synthesis construction

Optimal synthesis

We have to compute the switching curve \mathcal{S}

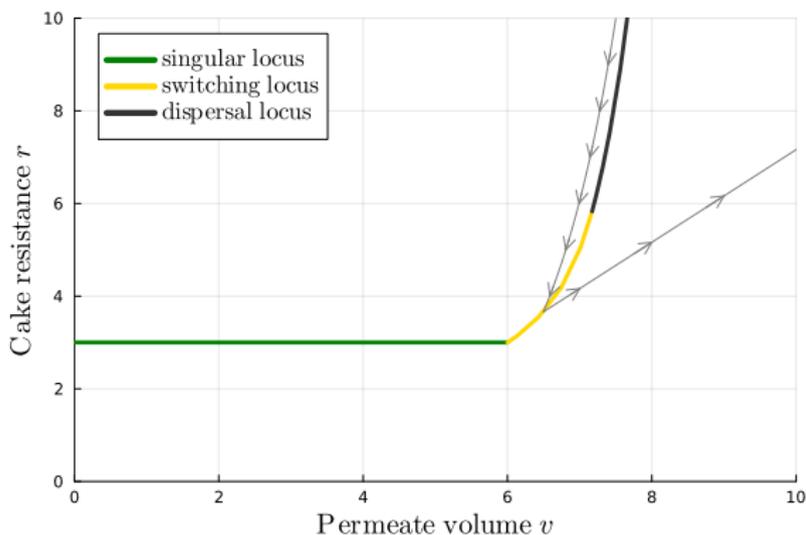


Figure: Optimal synthesis construction

Characterization of the switching curve

If $\xi = (x, y) \in \mathcal{S}$ then there exists $p = (-1, p_x, p_y)$ such that

$$H_0(x, p) = H_1(x, p) = 0 \quad \Rightarrow \quad p_x = \alpha(x) \quad \text{and} \quad p_y = \beta(x).$$

Moreover, denoting $\exp_{\vec{H}_+}$ the exponential map associated to the Hamiltonian vector field \vec{H}_+ generate by $H_+ = H_0 + H_1$ which stops when $y = y_f$, one has

$$\pi_{p_x}(\exp_{\vec{H}_+}(\xi, p)) = 0.$$

where $\pi_{p_x}(\xi, p) = p_x$. If $(x, y) \in \mathcal{S}$ then it is a zero of the function $S_{\mathcal{S}}: \mathbb{R}^2 \rightarrow \mathbb{R} = 0$ defined by

$$S_{\mathcal{S}}(x, y) = \pi_{p_x}(\exp_{\vec{H}_+}(x, y, p_x(x), p_y(x)))$$

Optimal synthesis

We have to compute the dispersal curve \mathcal{D}

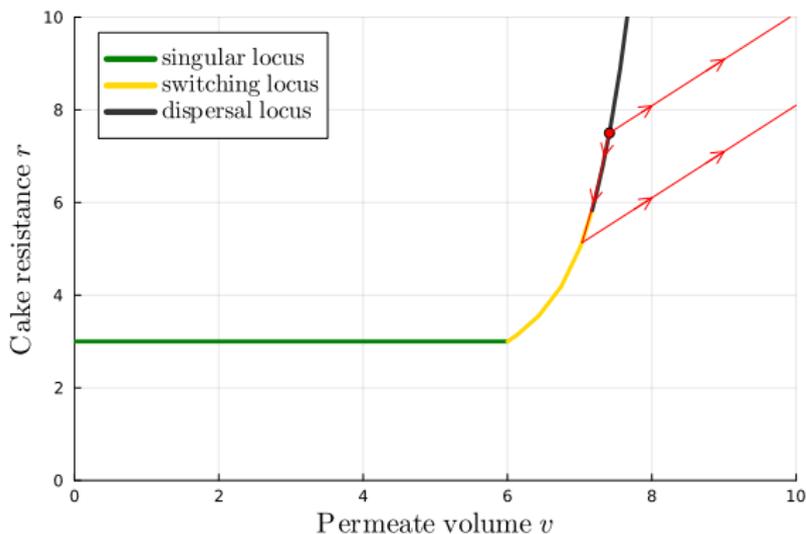


Figure: Optimal synthesis construction

Characterization of the dispersal curve

If $(x, y) \in \mathcal{D}$ then it is a zero of $S_{\mathcal{D}}: \mathbb{R}^2 \rightarrow \mathbb{R}$ defined by

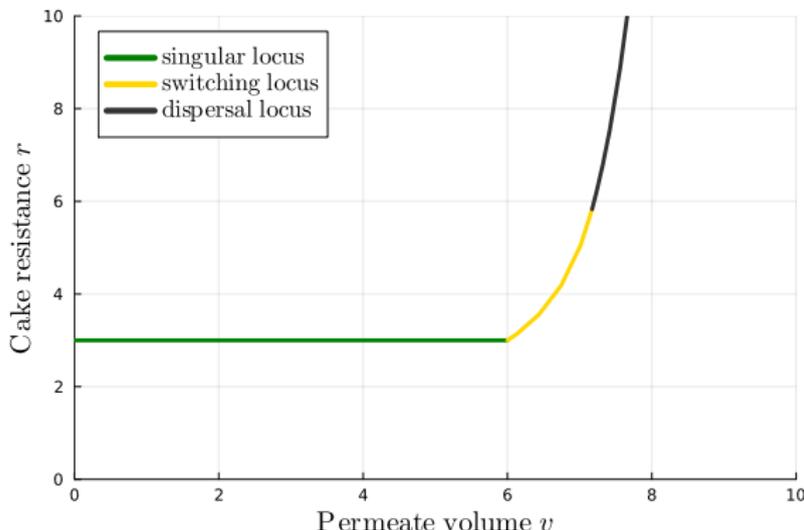
$$S_{\mathcal{D}}(x, y) = J(\gamma_+(x, y)) - J(\gamma_{-+}(x, y))$$

where :

- $\gamma_-(x, y)$ is the trajectory with the structure σ_- starting from (x, y) and stops when $y = y_f$,
- $\gamma_{-+}(x, y)$ is the trajectory with the structure $\sigma_- \sigma_+$ starting from (x, y) , stops when $y = y_f$ and switch on the switching curve,
- $J(\gamma)$ corresponds to the cost associated to the trajectory γ .

Switching and dispersal curve

The switching and the dispersal curves are the solution of $S(x, y) = 0$, where S is a function $S: \mathbb{R}^2 \rightarrow \mathbb{R}, (x, y) \mapsto S(x, y)$. Moreover, for both of them, we know an initial point (a, b) such that $S(a, b) = 0$



Differential continuation method

Let us suppose that there exists a function $\varphi(x)$ such that

$$S(x, \varphi(x)) = 0.$$

Since S is constant, we have

$$\frac{\partial S}{\partial x}(x, \varphi(x)) + \frac{\partial S}{\partial y}(x, \varphi(x)) \varphi'(x) = 0$$

Function $\varphi(x)$ is the solution of the ODE

$$\varphi'(x) = - \left(\frac{\partial S}{\partial y}(x, \varphi(x)) \right)^{-1} \frac{\partial S}{\partial x}(x, \varphi(x)), \quad \varphi(a) = b.$$

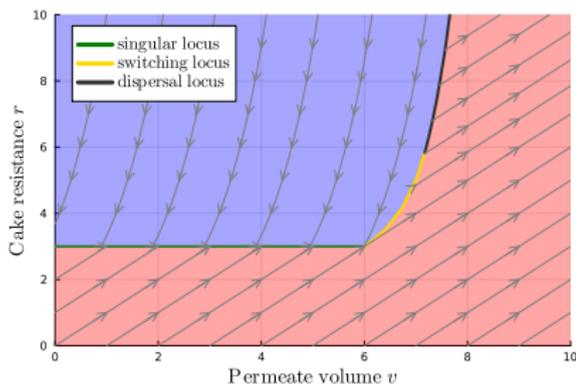
Differential continuation method

In Julia, packages **ForwardDiff** and **OrdinaryDiffEq** work together.

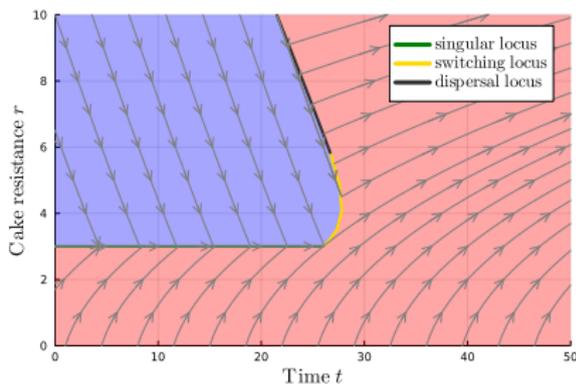
- The gradient of S is computed thanks to the **ForwardDiff** package.
- Even if S contains a solution of an ODE, the derivative of S is computed properly (it uses variational equations).
- The numerical integration is stopped when a condition is satisfied by using **Callback**.

Conclusion

We can generate automatically optimal feedback map associated to Problems in the form of (OCP), used for membrane filtration systems.



(a) Case (#1)



(b) Case (#2)

Conclusion

This framework can also be applied on more complex example, with non-connected singular locus.

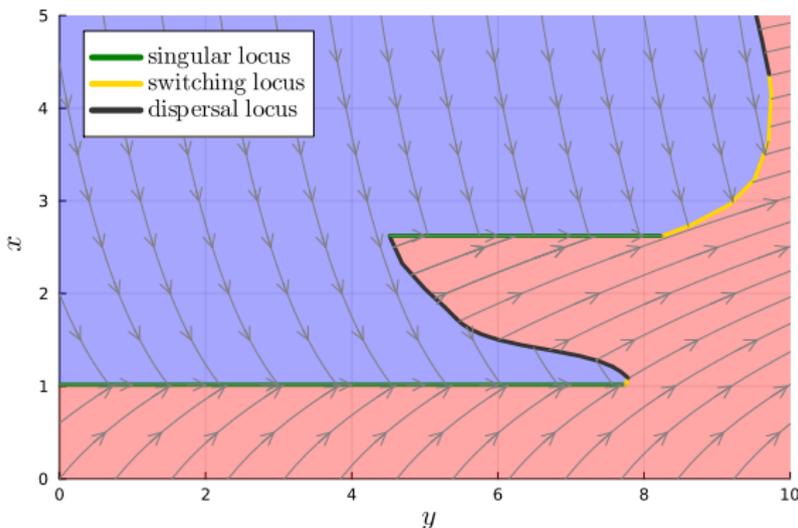


Figure: Toy example with non-connected singular locus.

References

Filtration.jl Package : Documentation and more examples

References :



Aichouche, F., Kalboussi, N., Rapaport, A., and Harmand, J. (2020).

Modeling and optimal control for production-regeneration systems - preliminary results -.
In 2020 European Control Conference (ECC).



Dutto, R., Harmand, J., and Rapaport, A. (2026).

Optimal control synthesis for a class of production-regeneration systems -Application to membrane filtration.



Kalboussi, N., Rapaport, A., Bayen, T., Amar, N. B., Ellouze, F., and Harmand, J. (2019).

Optimal control of membrane-filtration systems.
IEEE Transactions on Automatic Control.



Miele, A. (1962).

Extremization of linear integrals by green's theorem.

In Leitmann, G., editor, Optimization Techniques, volume 5 of Mathematics in Science and Engineering, pages 69–98. Elsevier.



Vroman, T., Beaume, F., Armanges, V., Gout, E., and Remigy, J.-C. (2021).

Critical backwash flux for high backwash efficiency: Case of ultrafiltration of bentonite suspensions.
Journal of Membrane Science.

Thank you for your attention !

<https://remydutto.github.io/>